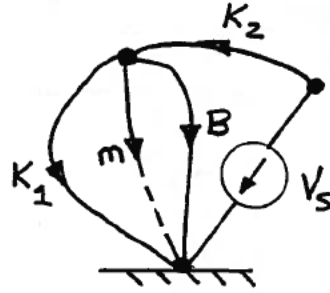
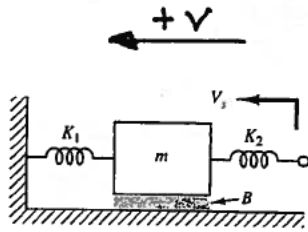


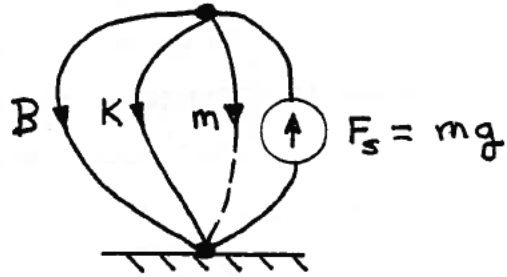
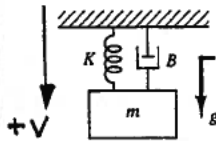
CHAPTER 4

PROBLEM 4.1

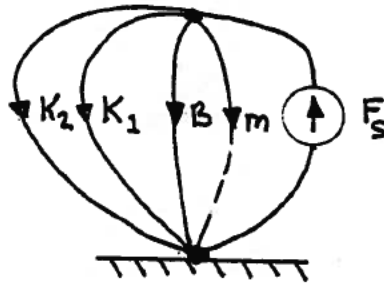
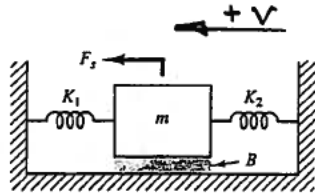
(a)



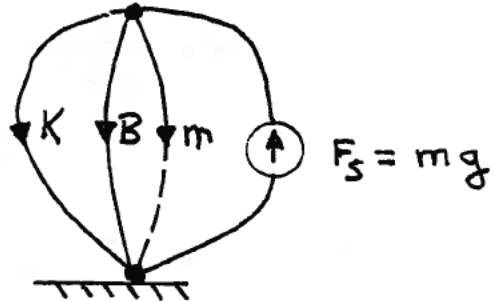
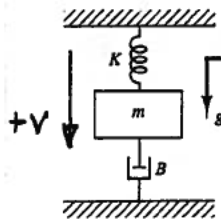
(b)



(c)



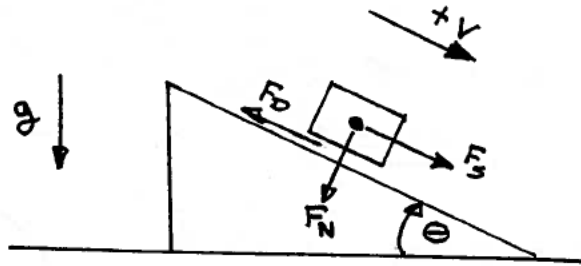
(d)



4-2

PROBLEM 4.2

(a)

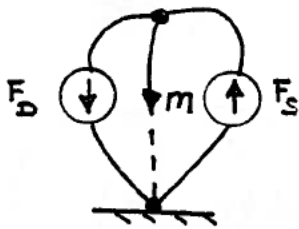


$$F_S = mg \sin \theta$$

$$F_N = mg \cos \theta$$

GRAVITY PROVIDES A FORCE F_S ALONG THE PLANE AND F_N NORMAL TO IT ACTING ON THE MASS. THE DAMPER FORCE F_D IS DUE TO THE FRICTION MATERIAL AND OPPOSES THE MASS MOTION

(b)



(c) AS θ INCREASES THE FORCE F_S INCREASES. AS FRICTION INCREASES THE FORCE F_D INCREASES

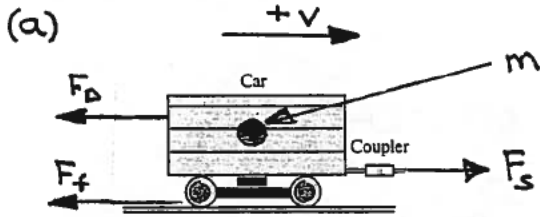
(d) For linear friction $F_D = Bv$
 At terminal velocity $v_T = \text{constant}$
 $\therefore \frac{dv}{dt} = 0$ AND $F_D = F_S$

$$Bv_T = mg \sin \theta$$

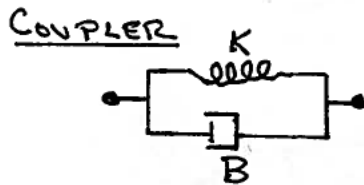
$$v_T = \frac{mg}{B} \sin \theta$$

4-3

PROBLEM 4.3

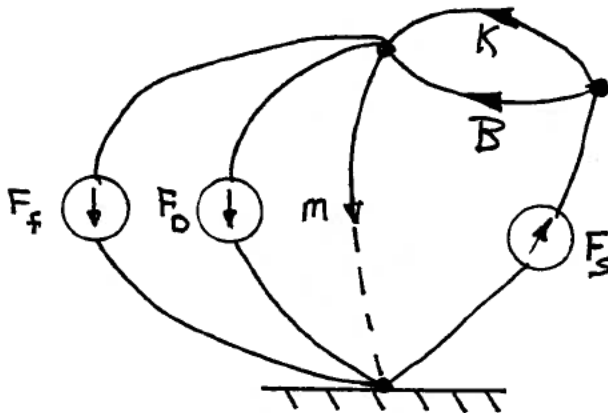


$F_s = F(t)$: LOCOMOTIVE
 F_f = TOTAL WHEEL FRICTION
 F_D = TOTAL AERODYNAMIC DRAG



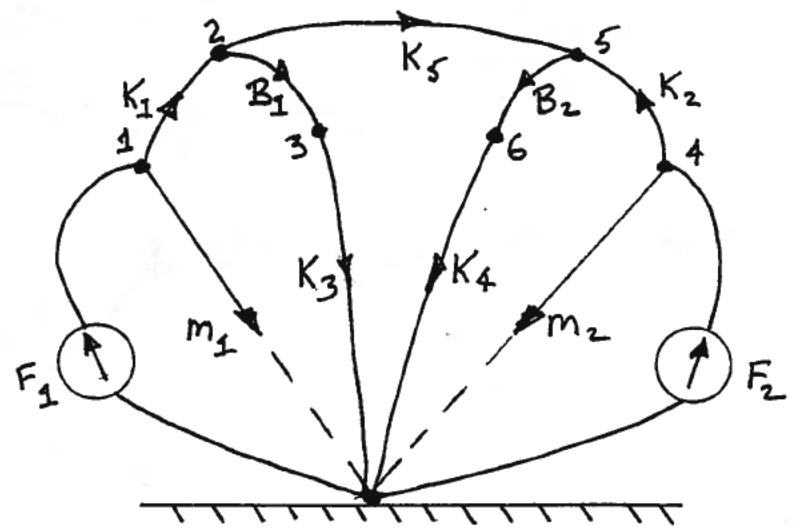
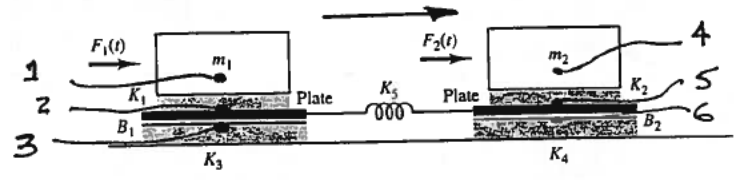
ELEMENTS IN PARALLEL OR ELSE COUPLER WOULD CONTINUE TO ELONGATE UNDER CONSTANT FORCE

(b)



PROBLEM 4.5

REFERENCE: +V

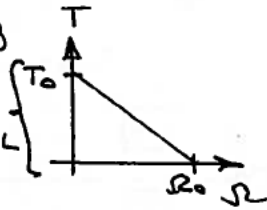


4-8

PROBLEM 4.8

(a)

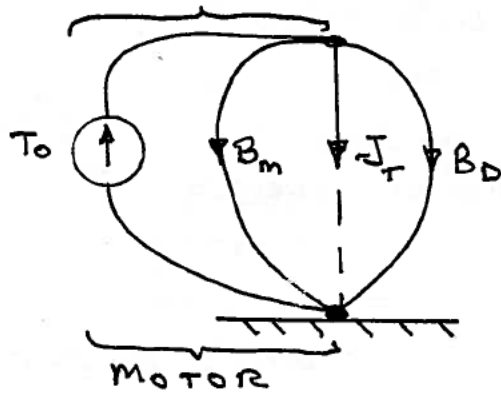
MOTOR MODEL



Source: T_0
DAMPER: B_m

- BEARINGS : DAMPER, B_D
- WHEN ASSUME MOTOR SHAFT VERY STIFF, then total disc plus motor inertia is J_T

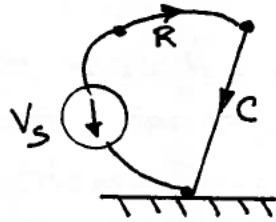
(b)



4-14

PROBLEM 4.15

(i) THÉVENIN SOURCE V_s, R



(ii) NORTON SOURCE I_s, R

